A Tool for Real-Time GNSS Performance Analysis in Air Traffic Management

Marco Brogi¹, Pierdomenico Tromboni²

ABSTRACT: This article introduces a numeric model, developed in a MATLAB environment, in order to monitor NAVSTAR GPS performances concerning accuracy effects and interference phenomenon. The model will be presented as a starting point for a future production of an open-source software, shareable and enlargeable, which will be able to provide real-time information about navigation satellite system performance. A sequence of analysis and comparisons with existing owners of the software will be possible using real data acquired with a high-performance monitoring station, in order to validate numeric models compiled.

KEYWORDS: NAVSTAR satellites, Air navigation, Multipath.

INTRODUCTION

The certification of Global Navigation Satellite Systems as tools able to provide to pilots and air traffic controllers a full support in all navigation phases could represent a real breakthrough for air traffic management (ATM), allowing the replacement of current navigation aids (such as NDB, VOR, DME, and ILS) with a single system able to provide the same navigation informations (on a global scale), according to the safety standards established by International Civil Aviation Organization (ICAO) for the different phases of flight (ICAO 2006). The adoption of a satellite system in the navigation phases will lead to the permanent revolution of airspace concept, with the free route becoming a reality: an airspace in which it is possible to choose different paths, thanks to the punctual knowledge of one's and others' position at all time, making it possible to plan a flight, optimizing time and fuel consumption and, therefore, bringing down mission costs.

CONTEXT AND OBJECTIVES

The most critical phase of flight is, as well known, landing. Safety standards set by ICAO for landing are very restrictive. Helicopters cruising and hovering also have critical phases due to the presence of much possible interferences at low flight altitude.

The target of this research is to provide a tool that is able to process data acquirable directly from satellites of global positioning system (GPS) constellation, in order to carry out a real-time monitoring of on-board navigation satellite system performances.

It is also known the importance of recognizing the quality and reliability of performances allowed by the navigation system in use, particularly during the most critical phases in flight, as slow-flying (take off and landing for an airplane as well as cruise and hovering for helicoper applications), for which different sources of errors – as interferences –, less considered during plain cruise, play a substantial role in terms of performance degradation.

Interferences could be caused by the presence of different sources of broadcast (for example, other navigation aids and also the presence of civil devices) or by undesired reflection of signal caused by orographic obstacles. This last type of interference is known as multipath and it can cause an error of about 2-3 m, which is negligible at high-flying but could be not admissible during a critical phase of flight such as landing or hovering for an helicopter.

Unlike civil aircrafts (both used as passenger transportation and freighter) that present a cruise altitude, in most cases, included in an interval of $9.000-11.000\,\mathrm{m}$, helicopters, as well as modern UAV systems, can fly at lower altitudes (150 m in empty regions and 300 m in urban areas) so, as a consequence, in these contexts, there is a greater probability that satellite signals are reflected by obstacles around.

Reduction of undesired error caused by multipath phenomenon (Ray 1999), together with application of satellite-based augmentation systems (SBAS) corrections in this branch (Oliveira and Tiberius 2008), could make possible a lot of operations that are not feasible at this time. In particular, it could be achievable to lead the low flying in safety in any orographic condition, e.g. low flying through mountains or wooded areas, both to make a local recon naissance and to provide rescue in areas not accessible otherwise.

A continous monitoring and the instant interferences mitigation would ensure the operative state of being contemporary

of general aviation aircrafts, rotorcrafts, and unmanned aerial vehicles (UAVs), for fire fighting and first-aid flights, first of all.

The increase in navigation satellite system accuracy and reliability could allow, in this context, to take advantage from terminal areas now unaccessible and, consequently, permit an intensive use of any type of strip.

In this paper, it is presented a MATLAB tool able to carry out a statistic postprocessing. Real data have been collected over a time interval of two months and then processed as better described in Table 1.

Acquisition campaign was conducted in an urban environment where a particular attention was directed to multipath effects which, as already mentioned, represent an important source of errors causing a degradation of position solution accuracy at low-flying. This tool represents a first step for the future development of a software able to process real data in real time, within totally open sources, and editable according with other user's demands. This flexibility and the possibility to share single modules with other users make this model really interesting.

METHODOLOGY

The study starts with a data collection campaign carried out with a fixed monitoring station located in an urban environment. Collected data were elaborated with an appropriate MATLAB

Table 1. Summary of cases of the study.

Stage	Duration	Objectives	Configuration	Form	ID reference
1	1 month	Accuracy evaluation and integrity monitoring/ comparison between two different configurations	2 Rx and 2 antennas 1 Rx able to receive only GPS signals 1 Rx able to receive both GPS signals and SBAS signals	Position form/ integrity form	ST.1
2	48 hours	Evaluation of multipath mitigation tool/comparison between presence or not of smoothing	2 Rx and 2 antennas 1 Rx able to receive only GPS signal and multipath mitigation option ON 1 Rx able to receive only GPS signal and multipath mitigation option OFF	Position form	ST.2
3	3 days	Evaluation of the advantages obtainable from a multiantenna system in terms of multipath mitigation	1 Rx and 2 antennas Rx is able to receive only GPS signals (masking angle is set at 10°)	Multipath form	ST.3
4	15 days	Comparison with results obtained in ST.3	1 Rx and 2 antennas Rx is able to receive only GPS signals (masking angle is set null)	Multipath form	ST.4

numeric code compiled specifically to compute GPS navigation data in RINEX format. A comparison with the correct results achieved by the receiver software will be conduct in order to validate the model.

The results obtained with both computing methods will be compared with ICAO standards for non-precision approach and CAT-1 precision approach in terms of horizontal and vertical position accuracy required.

At the end, some considerations about the goodness of the software and an idea to enhance and extend its reliability and potentiality will be given.

In Table 1, the four different case studies conducted are listed, summarizing, for each receivers and antennas, settings and configurations, the duration of each acquisition stage and the aim of each dataset. In the last column, the relative MATLAB form used to process data is listed for each dataset.

MATLAB MODEL

After a long data collection campaign (described in detail in the next paragraph and summarized in Table 1), it was developed a numeric code able to elaborate unrefined data and to produce numeric and visual results.

We chose to compile this model inside a MATLAB environment taking our way on "The GPS EASY Suite", published in 2003 by the Danish researcher Kay Borre (Borre 2009). This MATLAB suite is of high quality but it shows a lot of limits expecially for its generalization capacity. Starting from Borre's suite, we produced a more sofisticated and generic MATLAB software to process GPS RINEX format daily data and achieve navigation solution for all different input files with the frequency of one solution per second for 24 h per day.

Model Architecture

Numeric code is divided into three indipendent modules:

- A model to compute receiver position.
- A model to compute integrity events and, consequently, protection levels values.
- A model to quantify effects caused by multipath interferences in terms of pseudoranges.

Position Form

As described in Fig. 1, there are some secondary scripts, each one carrying out an essential information, that work in the background, and they are activated from a unique main script that we call "point_position".

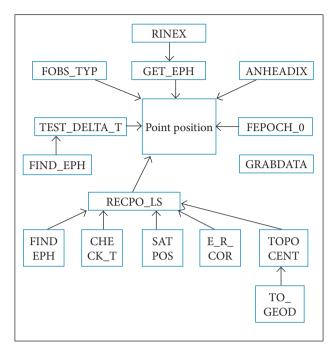


Figure 1. Position architecture.

Substantially, this module acquires input data from RINEX navigation and observation files; it process them, then it computes, for any single observation, satellite positions (from ephemeris) and, consequently, the best geometry available from receiver's point of view. Through a least square method, it computes receiver position applying the classic navigation solution algorithm based on the difference between measured and calculated pseudoranges (Hegarty and Kaplan 2000).

The output of this form is the receiver's position determined by satellites in every daily instant.

Integrity Estimation Form

The architecture of this module is similar to the previous one, with a unique script inside where many secondary functions work in the background.

It is independent from the position module. In addition to point position, we add here two particular functions: one of these is able to solve parity method algorithm in order to carry out a receiver autonomous integrity monitoring (RAIM) process (D'Avanzo *et al.* 2006). The second particular script, denoted "Pfa", is also essential to carry out RAIM because it is able to give as output the false alarm probability trend and a matrix including threshold values necessary to the comparison with statistical test in order to produce fault detection process (Liu *et al.* 2005).

This form solves RAIM parity method algorithm determining, first of all, the presence or not of a possible failure (basing on maximum satellite slope principle) and flagging this event with a message; then, the application of parity algorithm permits to

Multipath Estimation Form

estimate protection levels (Salos Andrés 2012).

From the architecture complexity point of view, it is the most elementary script. The objective of this script is to obtain a tool that is able to compute the analytical model to estimate the error caused by the presence of multipath in terms of pseudoranges measures.

Two different scripts were developed: one to estimate multipath trend over an observation period of 24 h, taking advantage of different pseudorandom noises (PRNs) over the day, in order to cover it entirely, and the other to observe the variation of multipath effect on a single satellite in the course of different daily intervals during which the same vector is visible by antennas.

The outputs of these scripts are represented by two charts that show quantification (in meters) of the error caused by this interference phenomenon.

TEST BED

A series of data collections were carried out in order to analyze the performance of the GPS in terms of horizontal and vertical accuracy, system integrity, and multipath effects. Data were collected with a global navigation satellite system (GNSS) monitoring station, property of ENAV S.p.A., over a period of two months.

Monitoring Station Layout

Fixed monitoring station (Ingegneria dei Sistemi S.p.A. 2012) was installed in the ENAV S.p.A. headquarters in the centre of Rome. This location implies that GPS signal is probably affected by a substantial error caused by a multipath phenomenon due to the presence of many buildings.

Monitoring station was composed by (a pattern of this layout is shown in Fig. 2):

- Two receiving antennas NOVATEL brand GNSS750.
- Two GNSS receivers Septentrio brand (PolaRx_pro and AsteRx2eH_pro).
- A network switch (HP 3COM).
- A personal computer HP brand 8560W equipped with an external hard disk driver (HDD).
- A network switch Enterasys.

Antennas were installed on the top of the building's roof, approximately at a height slightly above half a meter from the roof planking level.

Receivers are both multi-frequency and, even though they are two different models, they are similar in respect to performance accuracy. The only difference between PolaRx_pro and AsteRx2eH_pro is represented by a characteristic of the second one, which is able to work also with two input antennas: this property allows the receiver to be able to compute real-time kinematic (RTK) positioning (this function is not used in this context).

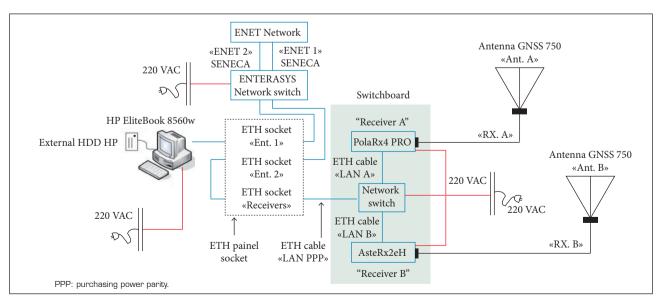


Figure 2. Monitoring station layout.

Antennas were characterized by a solid design and a low profile that make them ideal for a reference station that needs the presence of a sturdy antenna which ensures high performances. The antennas are both choke ring; in other words, they are omnidirectional high-frequency antennas, composed by a specific number of conductive concentric cylinder-shaped segments fixed near a central antenna. This type of antenna is particularly appropriate to receive satellite constellation signals and, above all, to mitigate multipath signals.

Data Collection

Acquisition campaign was conducted during the period between 21 May 2014 and 25 July 2014 and was divided into four different phases.

First Acquisition Stage (ST.1)

The first one was the longest phase. It started 6 June 2014 and ended after a month. In this phase, both receivers were used. The objective in this stage is to collect data to compare obtainable performances (in terms of position accuracy and integrity monitoring) between two different configurations: one based on GPS standalone configuration and the other that includes also the presence of satellite-based augmentation system (SBAS), in this case, represented by European geostationary navigation overlay system (EGNOS).

Second Acquisition Stage (ST.2)

Second, third and fourth phases were dedicated to the ability to analyze multipath phenomenon in an urban environment where our monitoring station is located.

In this stage the masking angle was set at 10° (the same used in a previous campaign). Both receivers were used, but in this case they were set to receive only GPS stand-alone signals. In order to analyze multipath errors that affect position solution accuracy, a different set of receivers was used. One receiver was set in order to be able to mitigate multipath, unlike the second one. In fact, both receivers can attenuate multipath errors through a post-processing estimate technique that allows to decrease the effects caused by reflected signals that are characterized by a small delay. This second acquisition phase was conducted over a time of 48 h.

Third Acquisition Stage (ST.3)

In this phase only one receiver was used: in particular, AsteRx2eH_pro was used because it is able to work with two input antennas. The objective in this phase is to evaluate the attempt to take advantage of a multiantenna system (Cannon *et*

al. 2000), then the multipath signal is revealed and closed off in terms of pseudorange and its measures are excluded before these fall within position solution computation (Grejner-Brzeziska and Vázquez 2012). The masking angle in this case is 5°, and the duration of stage was three days.

Fourth Acquisition Stage (ST.4)

The fourth and last phase is similar to the previous one. The difference between the third and this phase is represented by the masking angle setting, that is, in this case, null. In order to take advantage of daily periodic multipath event, the duration of the phase was set at 15 days.

PERFORMANCE EVALUATION

ICAO Annex 10 (2006) summarizes the performance values that a satellite system has to satisfy to be eligible as navigation aid for every phase of flight. In this context, we chose APV II category as reference performance values relative to non-precision approach and CAT I category relative to precision approach. Position errors are referred to antennas' geo-located positions.

Performances Relative to the First Acquisition Dataset

First acquisition dataset was processed with two different tools:

- MATLAB code already described.
- SBF Analyzer software (Septentrio receiver plug-in).

A comparison between the performed results was conducted.

Accuracy Performances (ST.1)

Septentrio Analyzer tool (Septentrio 2011) allows obtaining a qualitative analysis because it is possible to have results only in a graphic format and this allows getting only qualitative statistics. Accuracy statistics are expressed in terms of horizontal and vertical position error (HPE and VPE, respectively). Statistics daily values were obtained qualitatively from planimetric plots and approximated in order to reach a conservative situation.

In Fig. 3 daily statistics are plotted for horizontal and vertical accuracy for both configurations considered: stand-alone GPS and GPS with augmentation system.

As shown by charts, it is possible to note that the HPE (considering stand-alone GPS) is around 5 m. Only for a chance we see a greater value that, anyway, is in line with position error limits established by ICAO for APV II (horizontal accuracy is fixed at 16 m) and for CAT I approaches (same value).

Concerning vertical accuracy, stand-alone GPS is able to perform a vertical error around $6.5-7\,$ m, which is adequate for APV II approaches but does not fulfil requisites for CAT I precision approaches for which a maximum vertical error is established between 4 and 6 m. To satisfy this restriction it is necessary to consider the presence of an augmentation system. Adding EGNOS corrections, it is possible to reach a precision of $2-3\,$ m that is able to

It is interesting to note that Fig. 3 shows four values that move away from average error. In order to verify what could have caused these anomalies, a statistical survey was conducted.

satisfy CAT I requisites.

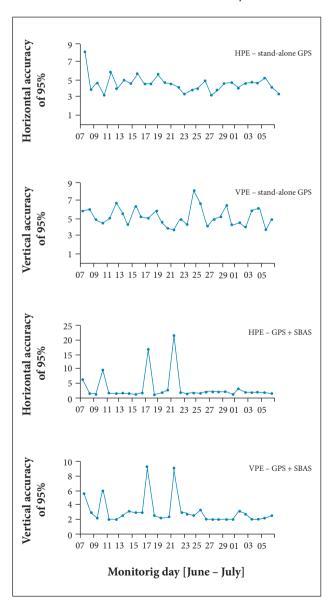


Figure 3. Horizontal and vertical accuracy statistics (ST.1).

In Fig. 4 position mode statistics are shown relative to one of these particular days (the other three are not presented but are very similar).

As we can note, position was not computed for all times considering EGNOS corrections: in some intervals, the receiver uses only GPS signals to compute position. Consequently, there were some disruptions of geostationary satellites, maybe caused by maintenance operations that caused loss of signal and succession of corrupted information broadcast.

To compare performances obtained from MATLAB model, we chose an opportune environment in terms of position accuracy.

In Fig. 5 coordinates trend (expressed in ECEF reference system), obtained processing daily RINEX files, is plotted. Ordinate reports coordinate errors compared to the reference point. It is possible to note that this error (for all three coordinates) shows a fluctuation around 20 m, which is five times greater than SBF Analyzer solution. It is clear that the implemented model is affected by systematics errors that cause this irregular trend and this substantial difference between the two solutions. We observed that this error does not show itself considering

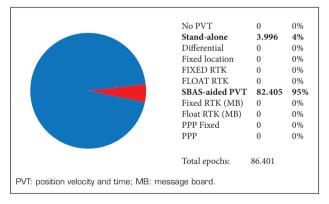


Figure 4. Position mode statistics.

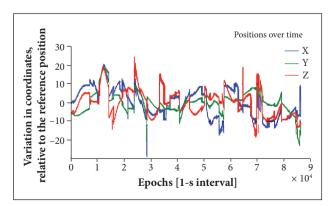


Figure 5. Matlab results of ECEF trend (ST.1).

short time intervals (that could represent the effective duration of a flight operation about 15 m). As a proof of that, in Fig. 6, two different examples of time intervals are plotted equal to 42 and 17 min, respectively. In these cases, position error shows a more regular trend in line with attended values. Thus the greatest problem is represented by the presence of error peaks that, systematically, caused up and down translations that make the solution unreliable and the model not appropriate yet to analyze data relative to long periods.

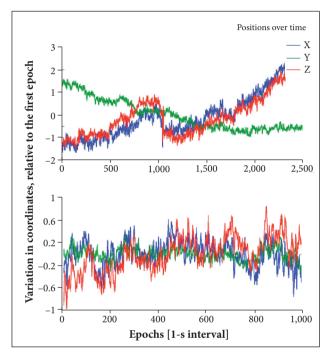


Figure 6. ECEF trend in two different time intervals (ST.1).

OBSERVATIONS: POSSIBLE ERROR REASONS

Scripts were debugged and it was checked that algorithms were implemented accurately. A first observation concerns an implemented position solution algorithm: it is based only on pseudoranges measures. It considers tropospheric errors, clocks syncronization errors and satellite propagation error but it totally ignores phase observation values which, as it is known, if added in the solution computation, allow to reduce error to centimeter size.

A second and more interesting observation concerns code basis. Looking at the plot in Fig. 5, it is possible to note how errors peaks appear, in some way, with a time uniformity, separating position value from reference geo-located position. Time intervals within maximum errors values seem to be equal to about 2 m. Then it is right to suppose that it could be a systematic error that shows itself every time the correction

parameters (relative to visible satellites) are upgraded. Taking for granted that correction parameters are correct, the origin of the error should be researched on the reliability of the orbital propagation algorithm used.

A comparison between the calculated satellites coordinates and the same coordinates provided directly by receiver shows that there is a difference of about $10^3 - 10^4$ m. A difference of this size moves to compute position referring to a satellite geometry substantially different from real configuration.

Integrity Performance (ST.1)

RAIM statistics derivable from receiver log files are provided in terms of these two parameters (Hewitson and Wang 2005):

- Horizontal external reliability level (HERL).
- Vertical external reliability level (VERL).

These parameters are described, respectively, as:

$$\begin{split} HERL &= max_{i = 1, \dots, m} \sqrt{\nabla \hat{x}_{E_i}^2 + \nabla x_{N_i}^2} \\ VERL &= max_{i = 1, \dots, m} \sqrt{\nabla x_{V_i}^2} \end{split}$$

subscripts E, N, and V represent local Eastern, Northern, and vertical coordinates; m is the number of possible alternative events.

External reliability represents the estimated parameter error that could be caused by a bias equal to minimum detectable bias (MDB). The system can be marginally protected using appropriate values of false alarm probability and missed detection probability. Thus external reliability level (ERL) can be confused with protection level even if it normally assumes a greater value than the corresponding protection level (PL); as a consequence, results will be more conservative in terms of safety.

If ERL > AL (alarm limit), there is the prospect that the quality of information could be compromised and, consequently, we could have a high integrity risk.

In Fig. 7 HERL/VERL data relative to both considered configurations are plotted and compared with specific AL values imposed by regulations for considered approach categories.

ERL is strictly dependent from constellation geometry, that is diluition of precision (DOP) value, both for horizontal and vertical cases. Looking at Fig. 7, it is possible to note that the system is satisfied by ICAO constraints in terms of reliability concerning horizontal case whereas vertical reliability levels (VAL) constraint is satisfied only for APV I approaches.

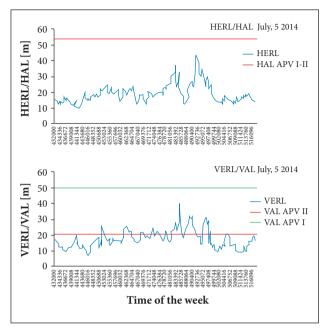


Figure 7. Horizontal and vertical reliability levels (HAL and VAL, respectively) in comparison with standard values (ST.1).

A comparison between performances obtained with MATLAB model was conducted similarly to accuracy case. Integrity estimation module already described allows to carry out RAIM function and to get protection levels values as a function of fixed false alarm probability. As seen in detail before, performances will be affected by a polarized error due to poor quality of the satellite propagation algorithm. Despite this, an analysis was conducted in particular to test the operation of computation code which results valid from an implementation point of view. In spite of systematic errors, horizontal protection level (HPL) values result lower than APV II alarm limit.

Multipath Effects (ST.2)

Multipath is one of the greatest error sources in both static and kinematic positioning. In particular, in such static applications, this phenomenon is particularly relevant because its effects are caused only by satellite dynamics and can produce therefore slow variation of systematic errors. For this study, the third MATLAB form previously described was used.

Three different phases of analysis were pushed through:

Considering different satellites in visibility over
24 h – a daily analysis of multipath error trend was carried out.

- A second stage analyzes the trend of error caused by multipath effects for a specified satellite in different moments of the day.
- The third and last analyses allow to perform a comparison in terms of masking angle effects.

Multipath Daily Effects on Pseudoranges Measure (ST.3)

The objective of this analysis is to quantify the error introduced by multipath that affects pseudoranges measure precision.

Because it is impossible to have a single satellite that is visible for consecutive 24 h, different satellites were considered as a function of their visibility time and their position over the horizon, in order to cover a daily interval. Error trend was analyzed for a week in order to have an adequate sample number.

Figure 8 shows that six different satellites were required to cover the entire daily visibility. The trend plotted in Fig. 8 is almost constant, and errors are included inside an interval of about 2 m. This result is in line with the goodness of the monitoring station configuration because, even though antennas are installed in an urban environment, they are placed on the roof of the buildings, so they are not affected by extreme reflections; for example, it is possible to find at the ground level the presence of the so-called urban canyon. Obstacles that the signals meet in their path are fixed. In addition we used choke ring antennas which are able to reject out-of-band signal until 50 dBc.

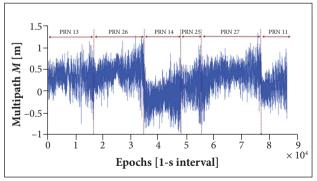


Figure 8. Multipath daily trend. Masking angle of the antenna is set at 10° (ST.3).

Multipath Effect on a Single Satellite

During a day, it is possible that the same satellite is visible more than once at a time. In this phase, different satellites were considered. In Fig. 9 a multipath error relative to satellite G06 is plotted as an example. In this case, G06 was visible by the station for three times in a day. First and second intervals are more significant to characterize the error behaviour; in fact, in these two cases, the satellite vector (SV) is locked for about 4 h without interruption.

In both cases, we can note how error shows a characteristic trend that follows proportionally the satellite trajectory from the observation point.

It is proven that multipath phenomenon appears, significantly, when a satellite is near the horizon and the signal path is more affected by the presence of obstacles in the surrounding environment.

The trend plotted in Fig. 9 confirms that. Indeed, it is possible to note that multipath error is about 2 m when it starts the lock between satellite and receiver (SV is near the local horizon); the satellite rises over the horizon and the error acquires a descendent trend oscillating around a value of 0.5 m. During dropping phase, error starts again to increase its value around 2 m or less.

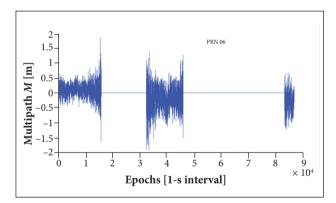


Figure 9. Multipath relative to a single satellite (ST.3).

Effect of Antenna Masking Angle

The trend described in Fig. 10 was obtained considering data relative to an acquisition conducted setting the masking angle equal to 0°. In this last phase, a comparison with the trend carried out using data relative to a 10-degree masking angle setup is conducted. Comparing this plot with the trend showed in Fig. 8, it is possible to point out differences relative to the effect of the considered interference.

A first observation concerns the number of satellites required to cover a 24-hour interval: with a masking angle of 10°, much satellites were used because the antenna rejects all signals broadcast by satellites characterized by a too small slope.

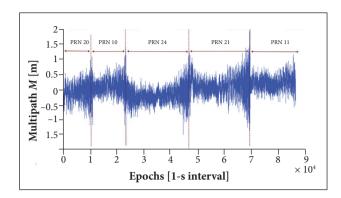


Figure 10. Multipath daily trend. Masking angle of the antenna is set as null (ST.4).

A second observation is that there is a difference in terms of error size. With 10°, the error is approximately 0.5 m smaller than the other case and reaches maximum values of about 1.5 m. This result is absolutely in line with attended values and confirms that, in an environment like this, where the monitoring station is located, with restricting antennas receiving radiation of a quantity equal to 10°, it is possible to have data less affected by errors caused by undesired reflections.

CONCLUSIONS

The MATLAB model presented in this article might be a first approach to the fulfilment of an open-source software produced to solve the problem of real-time monitoring of navigation satellite system performance. This software was expressly designed with a modular architecture in order to allow modifying and extending it in function of required applications. This modular architecture should lead to the extension of the software through the sharing of single modules developed on purpose by different users, creating a real community of users able to share their applications and results.

The next steps to carry out the development of a model that will be as more accurate and reliable as possible could be identified in a drop of processing data time, for example, using a simpler and optimized compilation of single scripts as well as, and in particular, the extension to other existing satellite constellations (Glonass, Galileo, and Beidou) in order to permit their interoperability that will run to an obvious improvement in terms of accuracy and availability of the full system.

In this context, a particular attention was directed to the analysis of GPS accuracy and the interferences caused by the presence of multipath phenomenon, particularly relevant concerning location of the monitoring station, so we developed modules for this type of applications. It would be desirable in the future to develop additional independent forms which will be able to perform a real-time analysis of, for example, additional interferences like the phenomena that could cause a performance degradation produced by navigation system leading to the employment of GNSS in ATM operations.

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